

#### Statens vegvesen

Norwegian Public Roads Administration

### Fire protection of tunnels - options and solutions

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Technology dep, Tunnel and concrete div.

# Fatal catastrophic fires has increased the focus on fire safety in tunnels

#### Fires in road tunnels

- Mont Blanc (F/I) 1999
  - 39 dead
  - 450 mill €
- Tauern (A) 1999
  - 12 dead
  - 50 mill €
- St. Gotthard (CH) 2001
  - 11 dead
  - ??? mill €





#### Fires in train tunnels

- King's Cross (GB) 1987
  - 31 dead
  - ??? mill €
- Baku (AZE) 1995
  - 289 dead
  - ??? mill €
- Eurotunnel (F/GB) 1996
  - 0 dead
  - 450 mill €
- Kaprun (A) 2000
  - 155 dead
  - 1.5 mill €/month















## There are obvious reasons to protect tunnels – but how?

### Fire load

- Fire size?
- Duration?
- Fire spread?
- Standards and codes?
- Experience?

. . .

• Testing methods?

### Fire resistance

- Structural design?
- Choice of materials?
- pp-fibers?

. . .

- External fire protection?
- Extinguishing systems?
- Fire suppression systems?

Type of tunnel (rock, cut and cover, immersed, floating, ...)

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Amount and type of traffic (%HGV, %DGV)

Ventilation

Technical equipment

Consequences for people and economy



## How are real fires represented as "numbers" for design of fire protection?

Truck and bus fires





### Commonly used time-temperature curves

- Standard ISO 834
  max 1030°C @2hrs
- Hydrocarbon (HC)
  max 1100°C @20min-2hrs
- RABT/ZTV
   max 1200°C @10-30min
- MHC

   max 1300°C @20min-2hrs
  - RWS - max 1350°C @1hr



K. Both, efectis



# What about experience with real scale fires or full scale fire tests?

- The UPTUN fire test in Runehamar Test Tunnel in 2003 clearly showed much higher HRR and gas temperatures than expected from normal HGV-goods
  - RWS-like temperatures
  - Up to 200MW
  - Fire can spread to vehicles 100m downstream
- Recent full scale tests performed by NPRA in Runehamar Test Tunnel showed that a small tanker-sized pool (11.000 liters diesel; 40m<sup>2</sup>) yields very high gas temperatures
  - Up to (more than?) 1400 °C
  - The ventilation was controlled by the fire



Gas temperature





	Heat Release Rates [MW]											
Fire category	Recommendations by institutions <sup>1)</sup>					Fire tests						
	PIARC		RABT	CETU (F)	NFPA 502	EUREKA	JREKA		Memorial:		Estimatos	
			(D)	Proposals <sup>2</sup>	(USA)	research:			adopted		from large	
			-	)					fire sizes		accidents <sup>6)</sup>	
	1987	1999	1994′′	1996/1997	1998	real fires <sup>3)</sup>	report				accidente	
							Ingarson					
Passenger car	5	2.5-8		2.5	5	1.5-2 <sup>4)</sup>	2.5-9					
Passenger car (large)				5								
passenger van (plastic)						5-6 <sup>5)</sup>					3-10	
1 – 2 passenger cars			5 - 10									
2 – 3 passenger cars				8								
1 van		15		15								
1 public bus		20				29-345)	29-34				36	
1 bus or 1 lorry (freight of	20		20 . 30	20	20				20			
lorry not hazardous)	20		20-30	20	20				20			
heavy goods vehicle				30		100-130°)	128				150-400	
petrol/gasoline tanker with a	100	100	50 - 100	200	100		20-100				120-300	
leak									50			
flammable spill of 400 liters									50			
flammable spillof 800 liters or									100			
hazardous material												
mixed load, 2844 kg, (wood,						15-17 <sup>5)</sup>						
rubber tyres, plastic material)												
different HGV loads								/1-223		_\		
carriage							12-47				3-100	

1): Dutch recommendations: see table 3.1/8

2): proposals are related to special types of road tunnels (e. g. with height clearance for passenger cars only, see table 3.1/9)

3): energy contents between approx. 3 GJ (passenger car) and approx. 90 GJ (heavy goods vehicle)

4): 3 fire tests done in Lappeenranta, Finland

5): values depend on the measuring system and on the method of data evaluation

6) Report Ingarson: [104]

7) New issue from 2003 [52] recommends fire loads for lorries only, depending on traffic:

- 30 MW if (lorries x km) / (day x table) ≤ 4000



Technical report Part 1 'Design Fire Scenarios'

75/161



## Design fires, Directives and codes – do they provide any answers?

- Full-scale fire tests (HGV and small-tanker) have proven to be very severe
  - Indications that RWS is not very conservative
  - Real fires (estimated) to larger than design fires

#### DIRECTIVE 2004/54/EC:

2.7. Fire resistance of structures

The main structure of all tunnels where a local collapse of the structure could have catastrophic consequences, e.g. <u>immersed tunnels</u> or <u>tunnels which can</u> <u>cause the collapse of important</u> <u>neighboring structures</u>, shall ensure a **sufficient level of fire resistance**....

No indication of fire loads...

No indication of what sufficient fire resistance is...

EN 1992-1-2:2004 Eurocode 2 -Structural fire design

- avoid collapse of the structure
- Valid "only" for ISO and HC fires
- Calculation models must be verified by fire tests for RWS, RABT, MHC...
- All relevant material data must be verified by fire tests for RWS, RABT, MHC...

No indication of fire loads for tunnels...

No standardized solutions or methods for the most severe fires...



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# Fire load on the walls must also be considered carefully – not only the roof!



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## It is critical to avoid spalling

- Explosive spalling is the most severe form of spalling
- Spalling can expose the reinforcement to high temperatures
- Spalling can reduce the load carrying capacity
- Spalling can lead to leakage of water (critical for immersed tunnels)
- Spalling can ultimately lead to a collapse of the structure







## Concrete looses strength and stiffness fast above 300°C





### Ultimately concrete melts above ~1200°C





SV-40 concrete started to melt after the FP failed



## Options for passive fire protection of concrete

## Improving the spalling resistance of concrete

- PP-fibers (type and amount !!)
- Steel fibers (type and amount !!)
- Aggregate (heat cap. and expansion)
- Porosity (the higher the better)
- Moisture (the lower the better)

## External fire protection as thermal barrier

- Protecting the concrete from strength loss
- Protecting the reinforcement
- Sprayed systems
- Board systems

Temperature requirements Spalling requirements Durability requirements Traffic load (anchoring, bond-strength, fatigue, ...) Aesthetics, surface finish, maintenance Easy replacement in case of damage



### PP-fibers are no guarantee for fire proofing!

#### 🔲 Comparison of Tunnel Segments



Fire Protection Engineering for New and Existing Tunnels - London - 6 October 2006

#### PP-fibers do not improve the thermal properties of concrete

PP-fiber concrete looses strength the same way as ordinary concrete



### Some examples of fire protection of tunnels

#### Holmsdale Tunnel, M25, London

- AADT 110,000; 6 lanes; divided traffic
- Concrete; cut and cover; buildings on top
- RWS; 200°C criteria for roof beams
- Cafco Fendolite MII (sprayed system) with mesh-reinforcement for roof beams





#### Clyde Tunnel; Glasgow

- Bored; under river; cast iron segments
- RWS; vibrations; curvature
- Promat Promatect-T (board system) with coated steel sheeting



## Fire protection of the Immersed Bjørvika Tunnel

- 300MW/RWS fire curve as design fire
- Development of a new test method for fire protection of concrete in RWS fire
- Both PP-fibers and thermal barrier
- Strict requirements for the external fire protection
- All systems must be mechanically anchored to the structural concrete
- Tender for roof/upper part of walls dead-line August 2008
- Tender for outer walls scheduled for publication late summer 2008
- ♦ Estimated cost 8-10 mill €





## Fire protection of the Immersed Bjørvika Tunnel – new test method

- Development of our own test method ٠ for fire protection of concrete in RWS
  - Based on fire testing of large concrete elements
  - RWS-proven systems failed in the larger scale test
- Compressive stress of 11 MPa
- High quality concrete (m=0.40, B55)
- Sealed curing, min. 3 months old
- Relatively large test elements (1.2 x 3.6 x 0.6 m<sup>3</sup>)
- Sprayed systems must be anchored with stainless steel mesh and bolts
- Board systems must have at least two joints
- 16 TCs for temperature at interface ٠ and at reinforcement



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## Fire protection of the Immersed Bjørvika Tunnel – concept of structural FP



- PP-fibers in the roof (lowest part, 30-40cm); 2kg/m<sup>3</sup>, 18um-6mm
- External fire protection on the roof and upper part of all walls; sprayed or boards; anchoring
- Sacrificial concrete wall element in outer walls (yet to be tested and verified)
- Calculation and measurements of temperature profile through sacrificial wall and in joints
- Special care taken at element and segment joints (movement) protect rubber gaskets and water-stop



## Fire protection of the Immersed Bjørvika Tunnel – strict requirements for FP

- Documentation acc. to TR no. 2494
- Fire resistance requirements
  - <u>No spalling</u> during/after tests
  - Interfacial temperature < 380°C</li>
  - <u>Reinforcement temp. < 250°C</u>
  - <u>No systems must fall off</u> during/after tests
- All parts must be non-combustible
- Sprayed systems must be anchored with stainless steel mesh and bolts
- Board systems must use stainless steel fixings
- Durability: carbonation, freeze/thaw, alkali-resistance
- Resistance against tunnel wash-down
- Fatigue; 150mill cycles;





### Summary

- Design fires for tunnels may not be conservative and they are not regulated in directives or standards
- No standards covering testing of fire protection of tunnels
- No standards or codes that give straight-forward solutions in case of RWS or similar large fire scenarios
- When collapse must be avoided a combination of PP-fibers and a thermal barrier is required
- Large fires require protection of roof
   and walls from top to bottom
- Pay attention to details!







### Thank you for your attention!

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